



Comparative Tensile and Shear Strength of Explosion Clad Materials

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COMPARATIVE TENSILE AND SHEAR STRENGTH OF EXPLOSION CLAD MATERIALS

TOPICS

- Background – Motivation for Test Program
- Experimental Design and Test Results
- Conclusions



Comparative Tensile and Shear Strength of Explosion Clad Materials

Background – Motivation for test program



BACKGROUND – MOTIVATION FOR TEST PROGRAM

- Cladding metal thickness typically too thin for tensile test coupon
- Clad specifications do not require clad tensile testing or identify minimum strength requirements
- Shear testing is common, but clad tensile strength data limited

| Shear Strength Specification Requirements | | |
|---|-----------------------------------|------------------------------|
| Clad Specification | Materials | Minimum Shear Strength (Mpa) |
| ASTM/ASME A263, A264, A265 | Stainless Steel and Nickel Alloys | 140 |
| ASTM B-432 | Copper and Copper Alloy | 85 |
| ASTM B-898 | Reactive Metals (Ti, Zr) | 137.9 |



WELD INTERNALS DIRECT

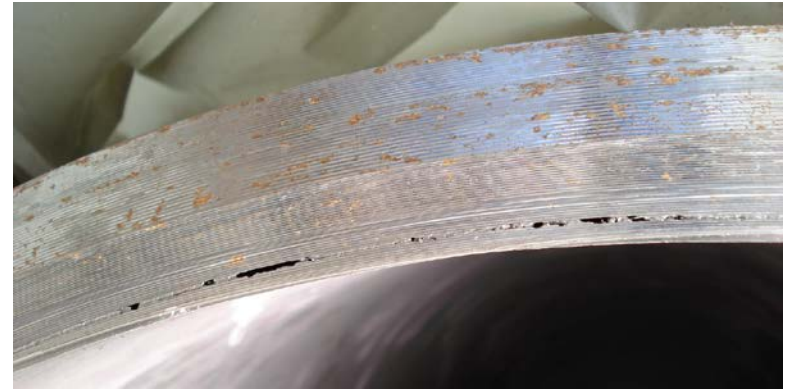
- Direct Welding Attachment of Internals
 - In clad vessels, internal attachments to the vessel wall are frequently required
 - Many companies require clad strip-back (especially for “heavy” internals)
 - Lack of data to support design
 - Concerns with clad separation



ADVANTAGES AND PROPERTIES OF EXW

1. Bond Quality

Disbonding of Roll Bonded Clad Plates
after forming and welding



X65Q 35.6 mm + Alloy 625 3.5 mm
OD 39", 90°/5D induction bend

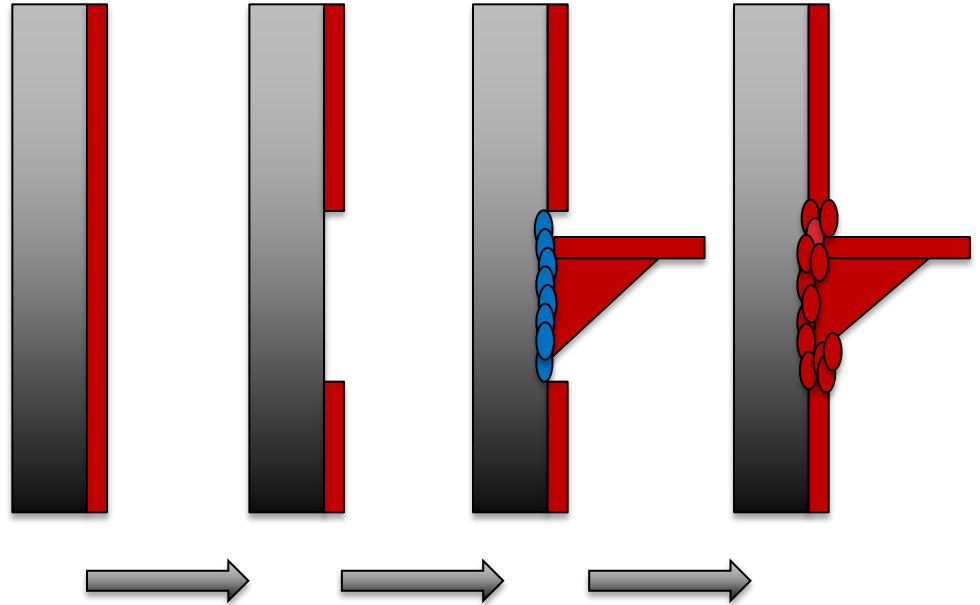
X65Q 31.1 mm + Alloy 625 3.1 mm
OD 53" (caisson)



Attachment with Clad Strip-back

Process Steps:

- 1) Strip back cladding
- 2) Inspect
- 3) Weld attachment to steel base metal (dissimilar metal weld)
- 4) Inspect
- 5) Complete CRA weld overlay
- 6) Inspect

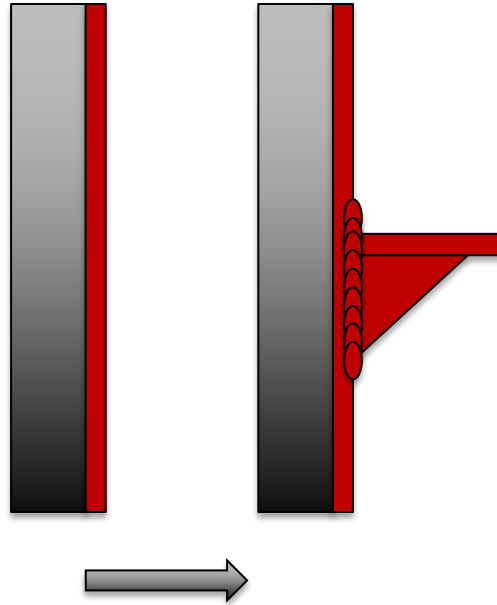


WELDING INTERNALS DIRECT

Direct Attachment with NobelClad EXW Clad

Process Steps:

- 1) Weld attachment directly to cladding metal
- 2) Inspect



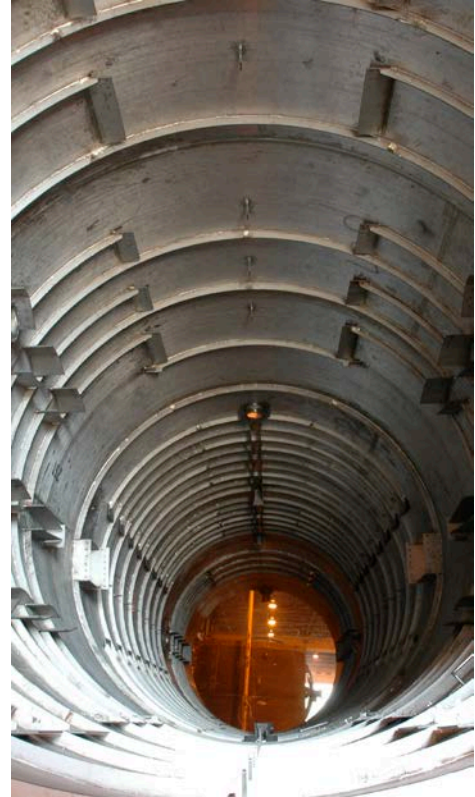
Direct Attachment

- Reduces cost \$\$\$
- Less time in shop
- No dilution or dissimilar metal welding
- Improves design flexibility



WELD INTERNALS DIRECT

- Direct Welding Attachment of Internals
 - Requires reliable, high strength cladding
 - Testing program initiated by NobelClad to investigate clad tensile strength



CRUDE DISTILLATION COLUMN
(Photo courtesy of Dacro Industries)



Comparative Tensile and Shear Strength of Explosion Clad Materials

Experimental Design and Test Results





EXPERIMENTAL DESIGN AND TEST RESULTS

- **Phase I**
 - Testing of a broad range of explosion clad production materials
 - Clad tensile strength is compared to the shear strength, and the cladding and base metal properties.
- **Phase II** describes a second series of tests focused on
 - Materials that are typical for oil & gas applications
 - Covers testing of coupons that simulate in-service conditions (welded coupons, SPWHT, elevated temperature testing, cantilever loading of welded attachment).



EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE I

- Test material selected from NobelClad production plates
 - Cladding metal thickness $\geq 9.5\text{mm}$
 - Heat treatment = production plate HT
- Tests machined from the same test block for direct comparison
 - Shear
 - Sub-size Clad Tensile (6.4mm gauge diameter)
 - Base Metal Tensile

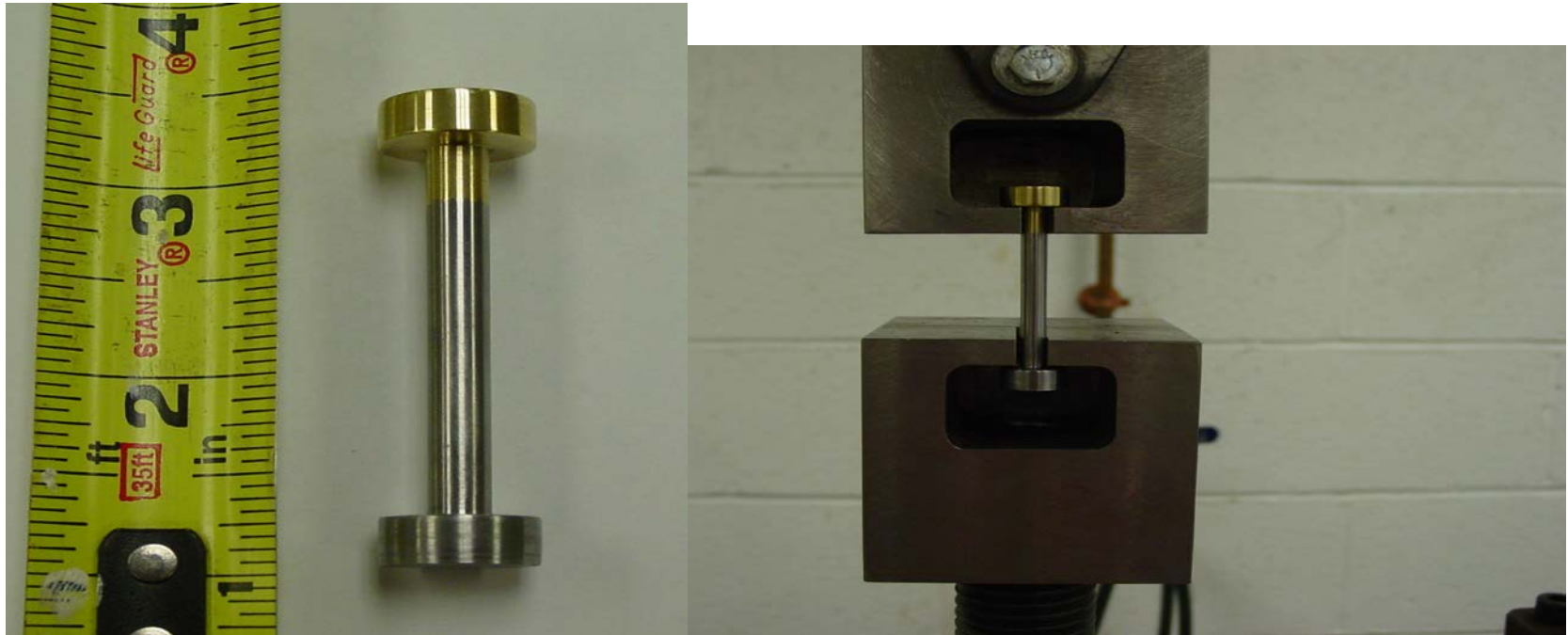


EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE I

| Clad Test Materials | |
|---|--|
| Cladding Metals | Base Metals |
| Stainless Steels / Nickel Alloys: 304L, 316L, 410S, Alloy 400, 2205, 2507 Duplex SS | SA 516-70 Carbon Steel |
| Copper Alloys: Naval Brass, 70-30 CuNi | SA 516-70 Carbon Steel |
| Titanium: Grade 1, 11, 17 | SA 516-70 Carbon Steel SA 266-4 Carbon Steel Forging SA 240-304L and 316L SS |



EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE I



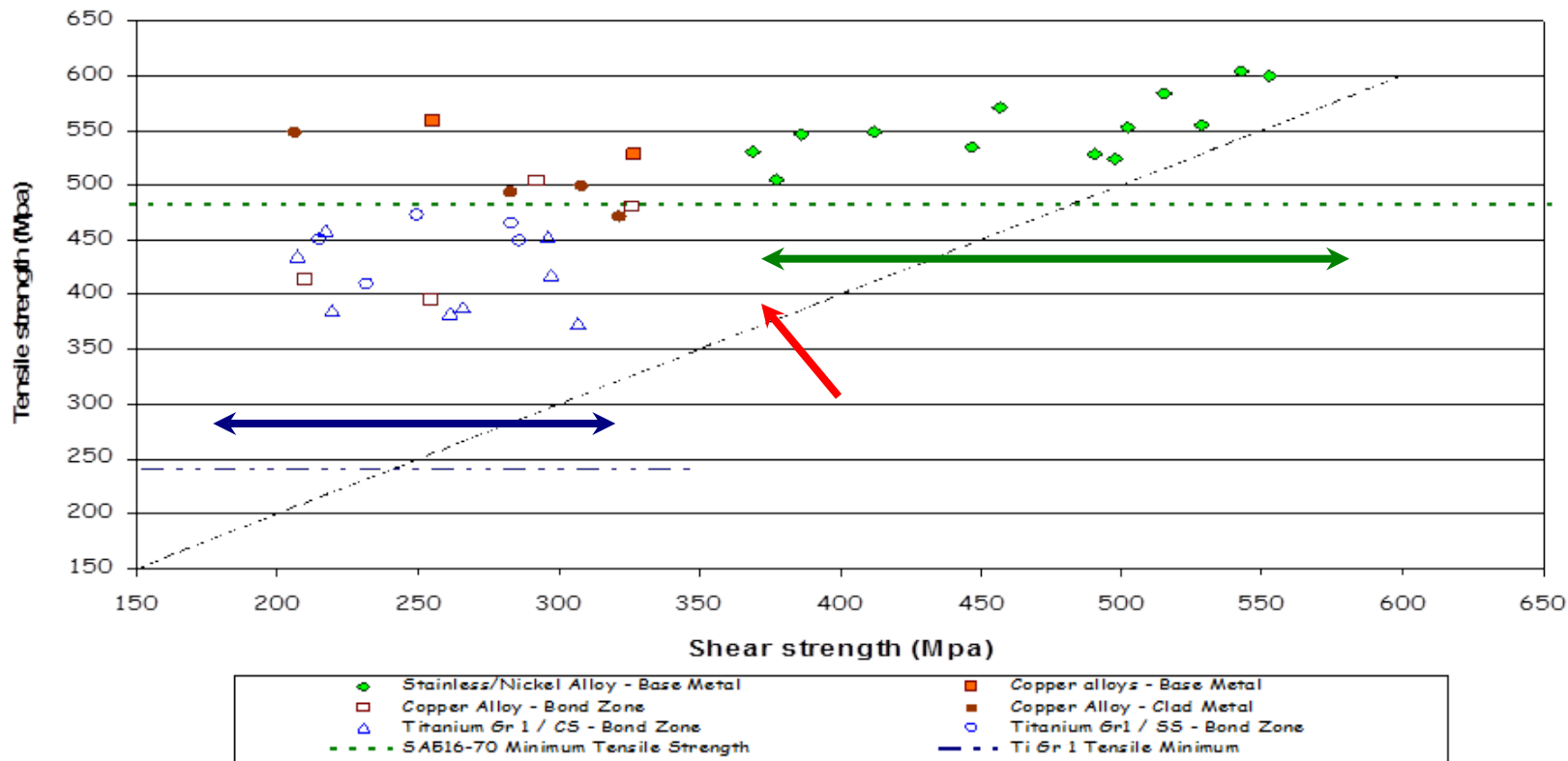
EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE I



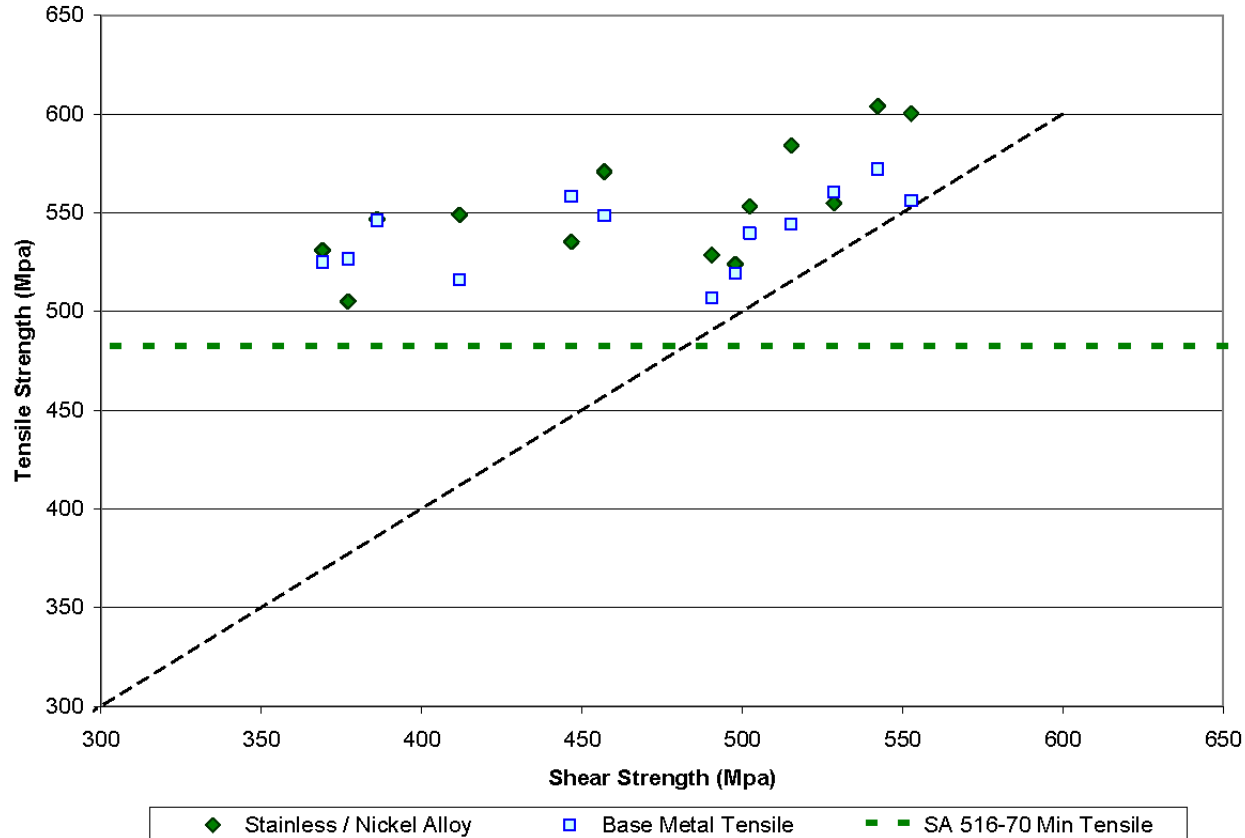
→ NobleClad.com



SHEAR STRENGTH VS. TENSILE STRENGTH



EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE I

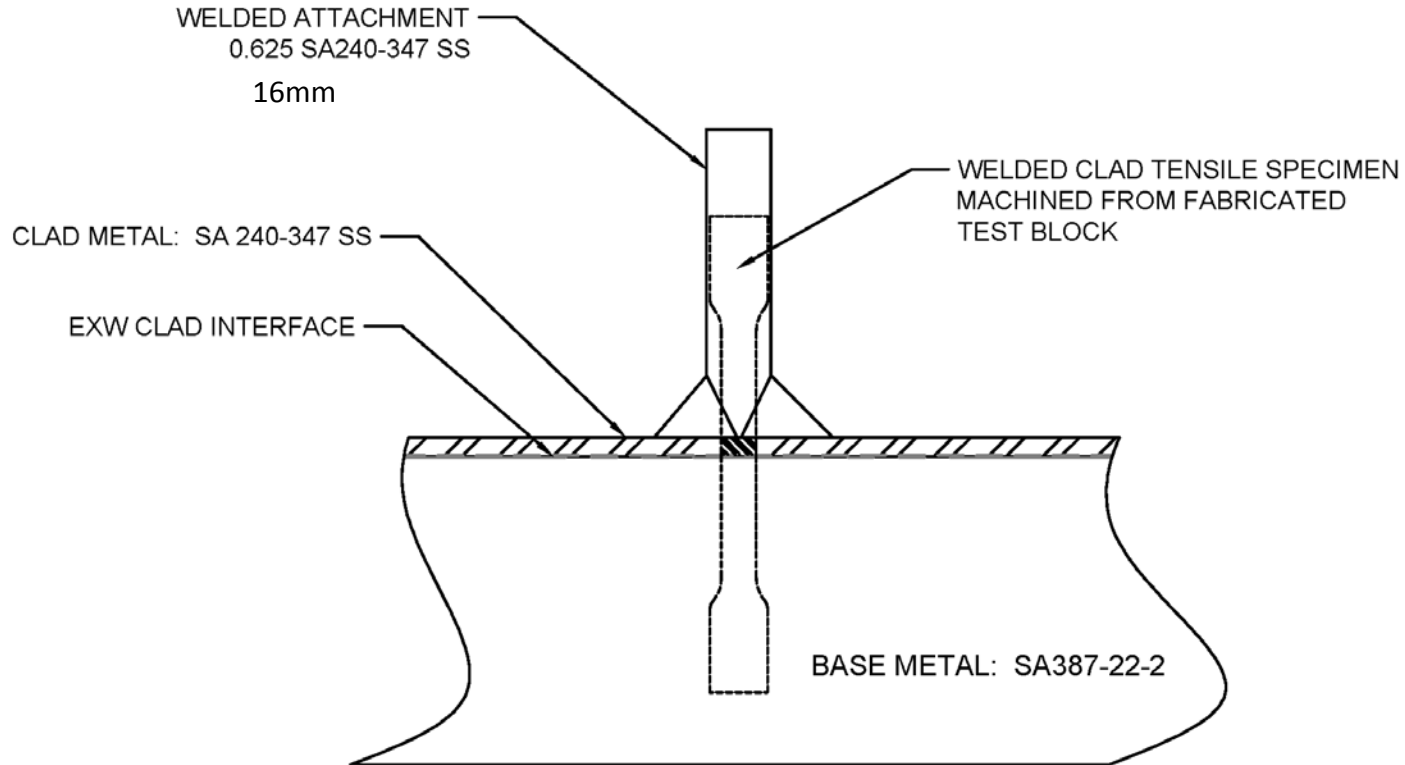


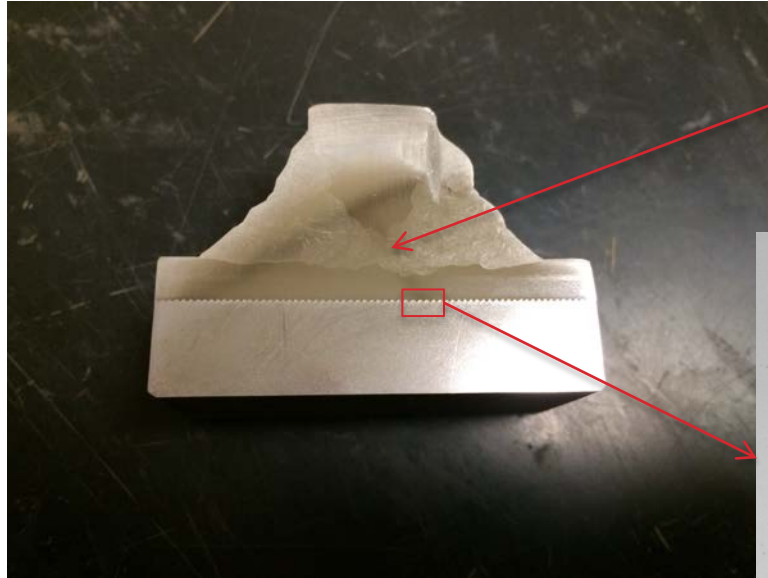
EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE II

- Covers testing focused on typical oil & gas materials and conditions
- Clad Tensile Testing
 - SA387-22-2, SA516-70 base metal
 - SA240-317L, -347 clad metals
 - 4.8mm cladding metal and welded test coupons
 - Elevated temperature testing (RT to 650°C)
 - Multiple cycles of SPWHT, step cooling heat treatments
 - Evaluation of Tensile Strength and HAZ with reduced cladding thickness
- Cantilever loading of welded attachment
- Tensile testing with simulated non-bond

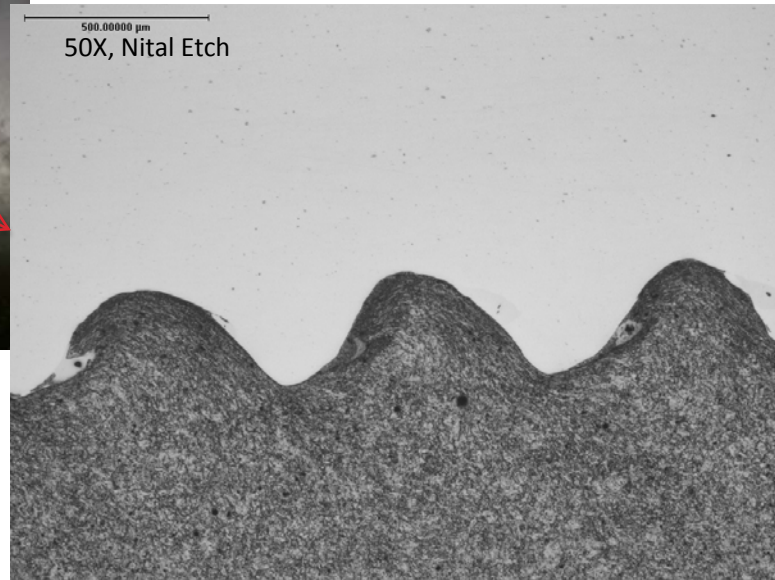


EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE II





Full penetration weld of
attachment
No change in steel structure
at bond interface



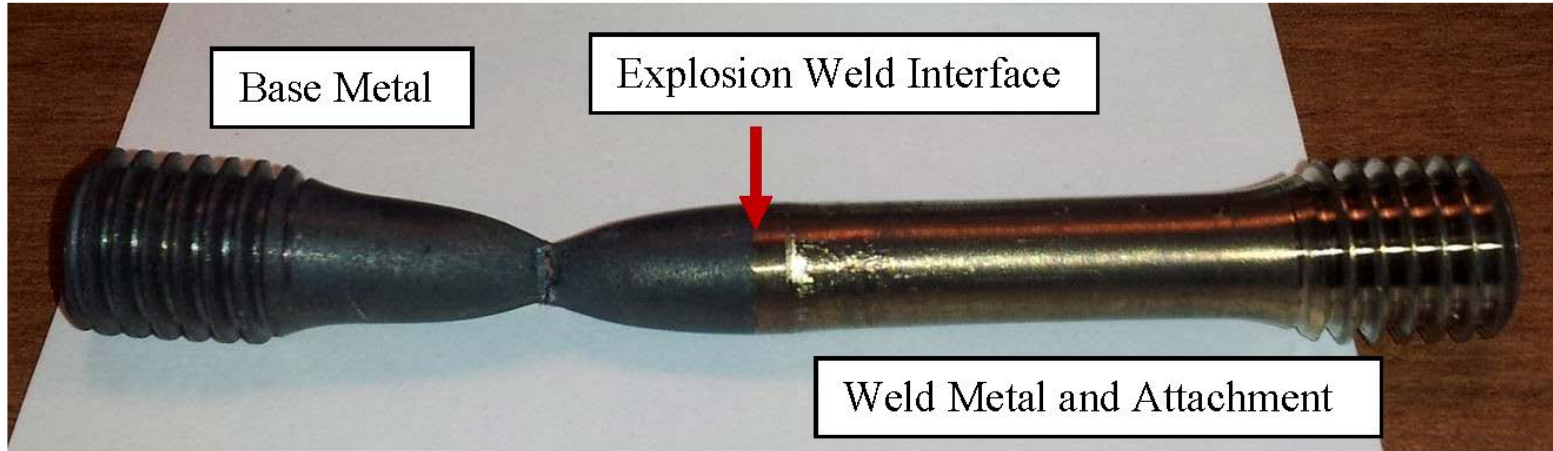
SA240-347 Clad
SA387-22-2 Base





EXPERIMENTAL DESIGN AND TEST RESULTS – PHASE II

- Clad tensile testing
 - Fractures in base metal



Test Temperature: 454°C (850°F)



Clad Tensile Testing (Welded Test Coupons)

RD13-0018

| Base | Clad | Condition | Sample ID | Test Temperature (°F) | Tensile | Yield | %Elong | %R.A. | Location of Fracture | |
|---------------------------------------|--|---|-----------|-----------------------|---------|-------|--------|-------|----------------------|------|
| SA516-70, 3.250" nom. thickness | SA 240-317L, 0.187" nom. thickness | As-Clad, As-Welded | A1-1 | Room Temperature | 78.1 | 48.6 | 15.0 | 35.1 | base | |
| | | | A1-2 | | 76.7 | 50.2 | 17.0 | 39.9 | base | |
| | | | A1-3 | | 77.7 | 49.3 | 14.4 | 33.6 | base | |
| | | | A2-1 | 500 | 64.5 | 32.1 | 24.1 | 79.1 | base | |
| | | | A2-2 | | 64.9 | 32.3 | 25.4 | 79.6 | base | |
| | | | A2-3 | | 64 | 34 | 25.5 | 79.8 | base | |
| | | | A3-1 | 850 | 56.5 | 31.1 | 19.7 | 49.1 | base | |
| | | | A3-2 | | 56.9 | 28.8 | 18.3 | 50.1 | base | |
| | | | A3-3 | | 56.5 | 35.0 | 17.6 | 44.9 | base | |
| | | | A4-1 | 1000 | 42.0 | 27.0 | 16.2 | 43.3 | base | |
| | | | A4-2 | | 42.3 | 26.8 | 17.9 | 44.6 | base | |
| | | | A4-3 | | 42.2 | 27.3 | 15.7 | 41.9 | base | |
| | | As Clad + SPWHT 1100°F, 120 min. Heating and cooling rates per UCS 56 | | Room Temperature | B1-1 | 76.6 | 51.0 | 17.7 | 40.4 | base |
| | | | | | B1-2 | 77.3 | 48.0 | 17.7 | 36.1 | base |
| | | | | | B1-3 | 76.5 | 47.1 | 17.0 | 34.4 | base |
| | | | | 850 | B2-1 | 55.6 | 26.7 | 19.7 | 45.0 | base |
| | | | | | B2-2 | 55.4 | 29.5 | 20.4 | 46.0 | base |
| | | | | | B2-3 | 56.9 | 31.1 | 19.6 | 43.6 | base |
| | | | | 1000 | B3-1 | 40.9 | 26.4 | 19.6 | 44.0 | base |
| | | | | | B3-2 | 41.2 | 26.2 | 20.1 | 43.6 | base |
| | | | | | B3-3 | 41.4 | 27.4 | 19.6 | 42.7 | base |



Clad Tensile Testing (Welded Test Coupons)

RD13-0018

| Base | Clad | Condition | Sample ID | Test Temperature (°F) | Tensile | Yield | %Elong | %R.A. | Location of Fracture |
|--|--------------------------------------|--|-----------|-----------------------|--|-------|--------|-------|----------------------|
| SA387-22-2 Q+T, 2.990" nom. Thickness | SA240-347, 0.187nom. thickness | As Clad + Post Clad SRHT 1175F, 120 min. (HT performed on plate - no further HT required), As-Welded | CI-1 | Room Temperature | 79.8 | 57.6 | 23.6 | 80.3 | base |
| | | | C1-2 | | 80.1 | 56.7 | 23.1 | 79.6 | base |
| | | | C1-3 | | 80.1 | 57.8 | 23.5 | 79.6 | base |
| | | | C2-1 | 850 | 62.3 | 42.4 | 22.2 | 77.5 | base |
| | | | C2-2 | | 62.4 | 41.7 | 22.9 | 77.7 | base |
| | | | C2-3 | | 62.4 | 40.4 | 22.8 | 78.9 | base |
| | | | C3-1 | 1000 | 54.5 | 39.0 | 22.6 | 83.5 | base |
| | | | C3-2 | | 54.6 | 39.0 | 22.4 | 82.9 | base |
| | | | C3-3 | | 54.3 | 42.5 | 22.9 | 83.3 | base |
| | | | C4-1 | 1200 | 39.3 | 33.2 | 29.0 | 89.9 | base |
| | | | C4-2 | | 39.4 | 31.7 | 28.8 | 90.3 | base |
| | | | C4-3 | | sample damaged during preparation - not tested | | | | |



Clad Tensile Testing (Welded Test Coupons)

RD13-0018

| Base | Clad | Condition | Sample ID | Test Temperature (°F) | Tensile | Yield | %Elong | %R.A. | Location of Fracture |
|---|---------------------------------------|---|-----------|-----------------------|---------|-------|--------|-------|----------------------|
| SA 387-22-2 Q+T, 2.990" nom. Thickness | SA 240-347, 0.187nom. thickness | + 1Cycle SPWHT 1274°F, 500 min. Heating and cooling rates per UCS 56 | D1-1 | Room Temperature | 78.4 | 55.6 | 24.0 | 79.7 | base |
| | | | D1-2 | | 78.5 | 55.3 | 23.8 | 78.8 | base |
| | | | D1-3 | | 78.5 | 55.3 | 24.6 | 79.5 | base |
| | | | D2-1 | 850 | 60.5 | 39.0 | 21.1 | 77.0 | base |
| | | | D2-2 | | 60.4 | 40.1 | 21.7 | 77.9 | base |
| | | | D2-3 | | 61.1 | 40.0 | 21.8 | 78.1 | base |
| | | | D3-1 | 1000 | 52.1 | 39.9 | 22.9 | 82.4 | base |
| | | | D3-2 | | 52.4 | 38.2 | 23.9 | 82.7 | base |
| | | | D3-3 | | 52.4 | 40.4 | 23.6 | 83.3 | base |
| | | | D4-1 | 1200 | 37.6 | 31.6 | 29.6 | 90.4 | base |
| | | | D4-2 | | 37.7 | 31.2 | 11.6 | 29.1 | weld |
| | | | D4-3 | | 37.5 | 31.0 | 17.8 | 41.9 | weld |



Clad Tensile Testing (Welded Test Coupons)

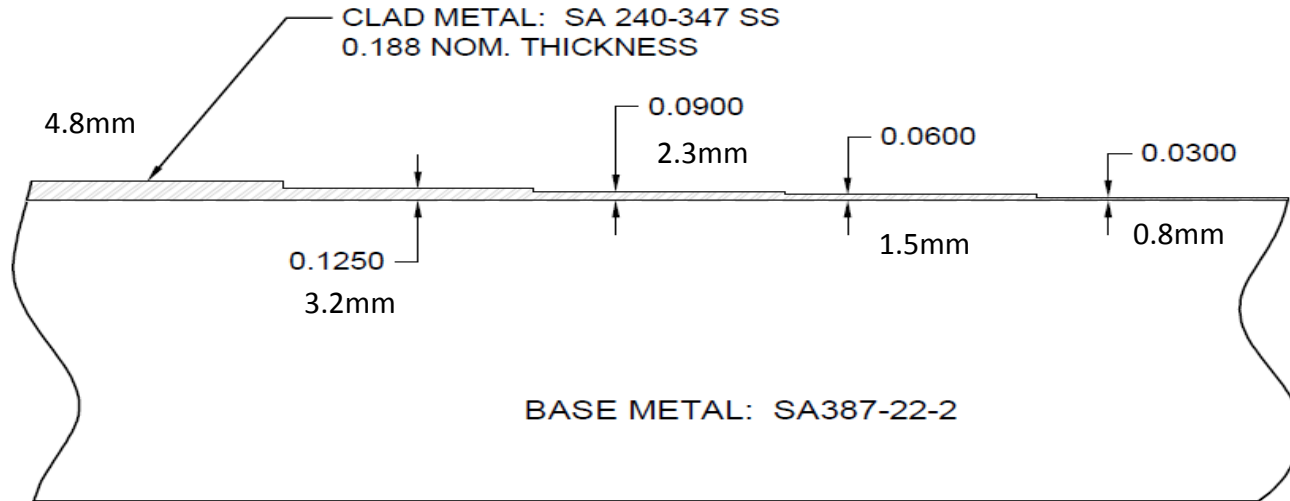
RD13-0018

| Base | Clad | Condition | Sample ID | Test Temperature (°F) | Tensile | Yield | %Elong | %R.A. | Location of Fracture |
|--|--------------------------------------|---|-----------|-----------------------|---------|-------|--------|-------|----------------------|
| SA387-22-2 Q+T, 2.990" nom. Thickness | SA240-347, 0.187nom. thickness | +3 Cycle SPWHT 1274°F, 500 min. (1500 min. total) Heating and cooling rates per UCS 56 | EI-1 | 850 | 60.0 | 39.3 | 21.0 | 78.1 | base |
| | | | EI-2 | | 60.0 | 36.7 | 20.9 | 77.7 | base |
| | | | EI-3 | | 60.1 | 37.4 | 20.5 | 77.3 | base |
| | | | E2-1 | 1200 | 36.3 | 29.1 | 28.4 | 91.0 | base |
| | | | E2-2 | | 36.5 | 29.0 | 29.1 | 88.8 | base |
| | | | E2-3 | | 36.5 | 29.7 | 28.7 | 90.6 | base |
| | | +1Cycle SPWHT 1274°F, 500 min. Heating and cooling rates per UCS 56 +SA-387 S63.2 Step Cooling | F1-1 | 850 | 58.2 | 38.4 | 20.9 | 78.0 | base |
| | | | F1-2 | | 58.5 | 43.1 | 22.3 | 78.7 | base |
| | | | F1-3 | | 57.9 | 38.5 | 20.3 | 78.0 | base |
| | | | F2-1 | 1200 | 37.1 | 31.3 | 29.9 | 90.9 | base |
| | | | F2-2 | | 35.3 | 26 | 30.6 | 90.4 | base |
| | | | F2-3 | | 37.3 | 30.9 | 28.6 | 90.7 | base |



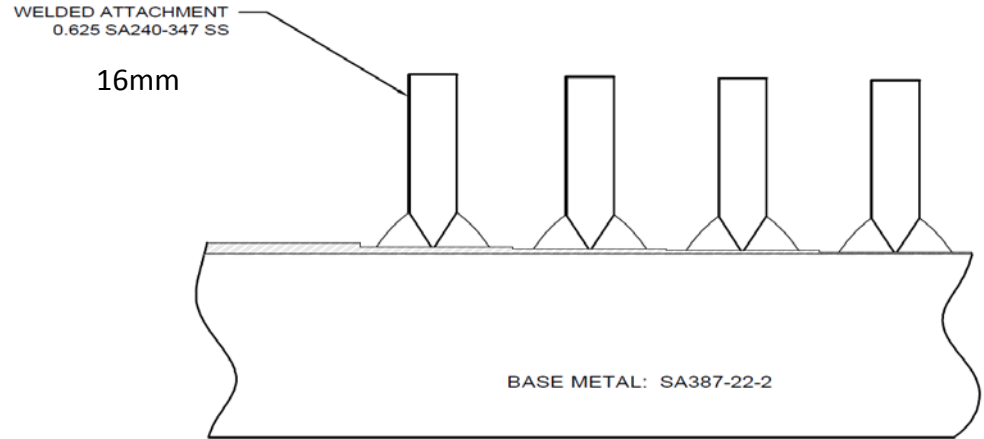
EVALUATION OF TENSILE STRENGTH AND HAZ WITH REDUCED CLADDER THICKNESS

- Evaluate minimum clad thickness required for direct attachment welding without affecting the base metal
- Demonstrate tensile properties without PWHT



TEST SET UP AND TENSILE RESULTS

- 4.8mm Clad: 593 MPa
- 3.2mm Clad: 589 MPa
- 2.3mm Clad: 598 MPa
- 1.5mm Clad: 590 MPa
- 0.8mm Clad: 610 MPa



- All failure locations were in the SA 387-22-2 base metal

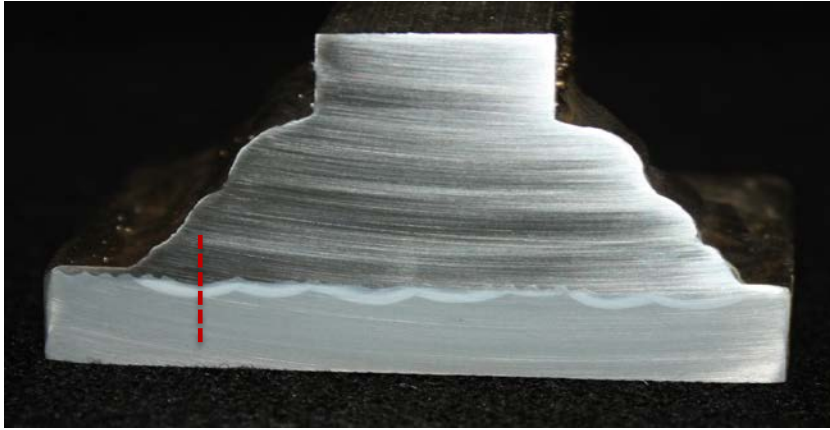


WELDING PARAMETERS

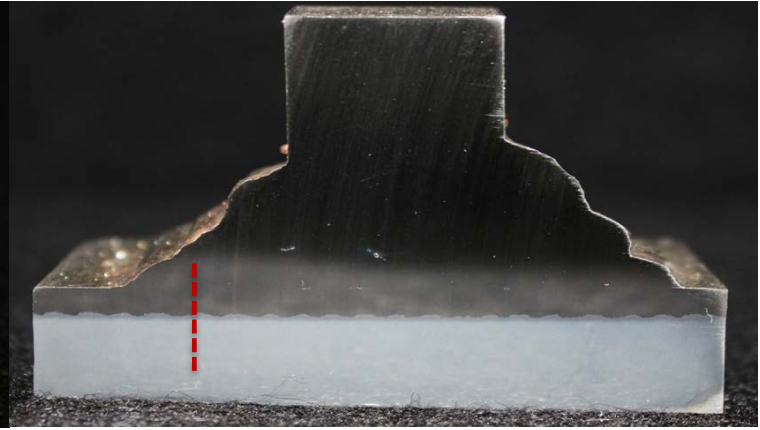
- Process: GMAW
- Shielding Gas: 90% He, 7.5% Ar, 2.5% Co2
- Filler Metal: ER347
- Current: 181 Amps
- Voltage: 21 Volts
- Travel Speed: 10 IPM
- Wire Feed Speed: 350 IPM
- Heat Input: 22,806 Joules per inch



EVALUATION OF HAZ



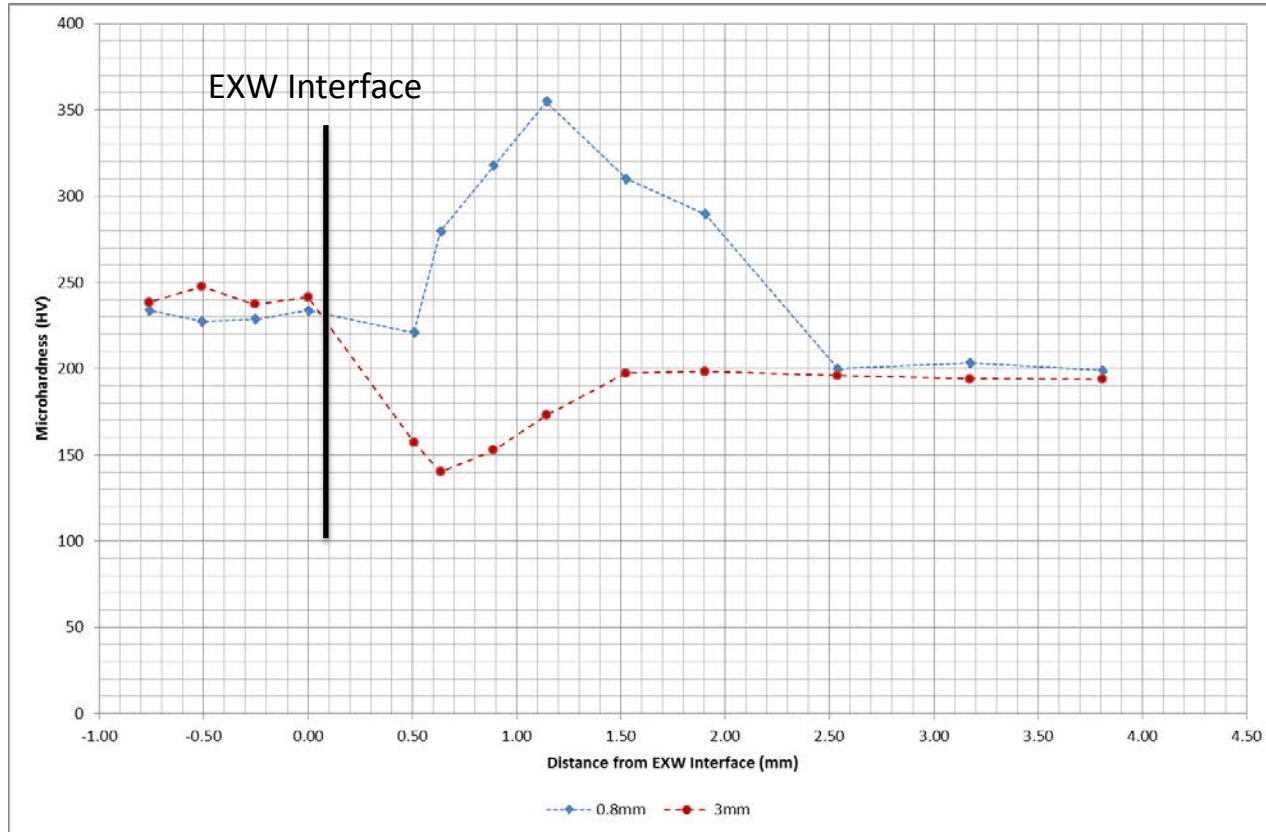
0.8mm Clad Thickness



3.2mm Clad Thickness



EVALUATION OF HAZ

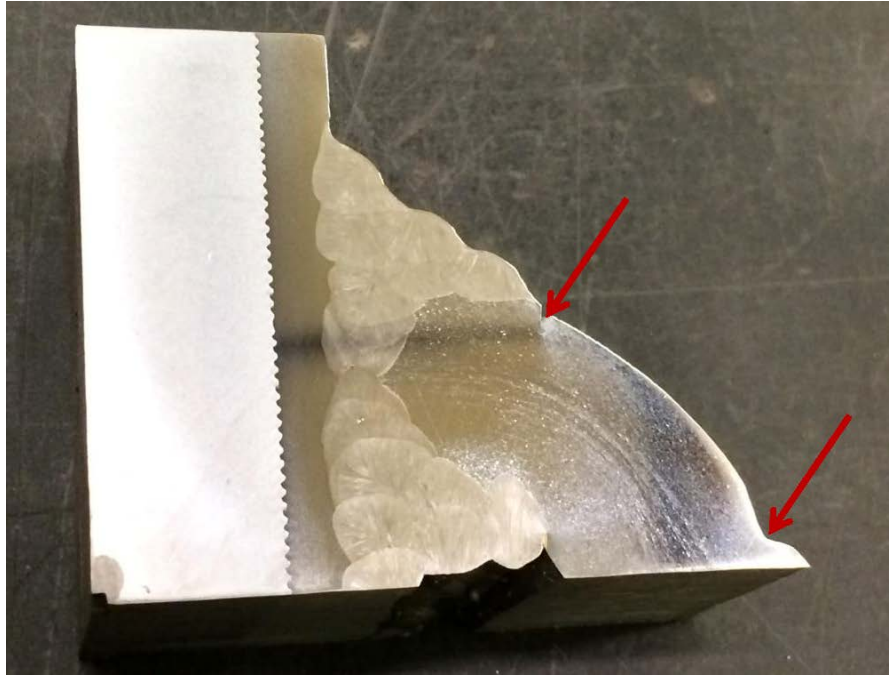


CANTILEVER LOADING OF WELDED ATTACHMENT

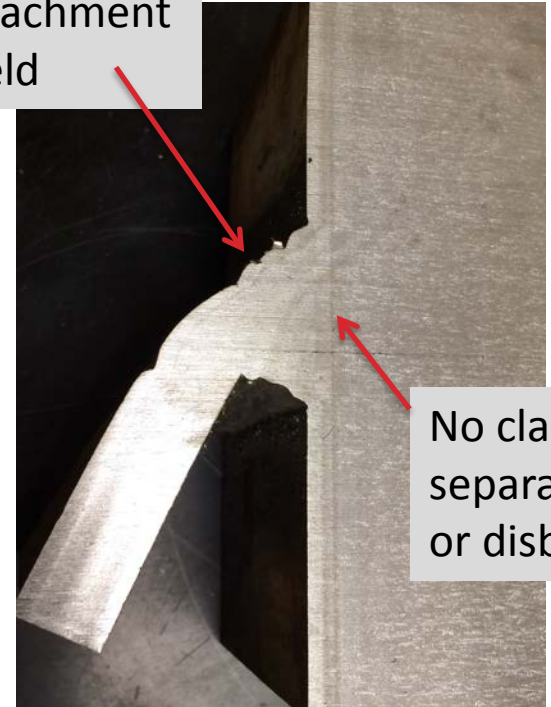
- Application mock-up testing
 - Bending moment on a welded attachment.
 - Loaded to failure on the production press.
 - After loading , samples cut for metallographic examination and evaluation.



CANTILEVER LOADING OF WELDED ATTACHMENT



Cracking in
attachment
weld

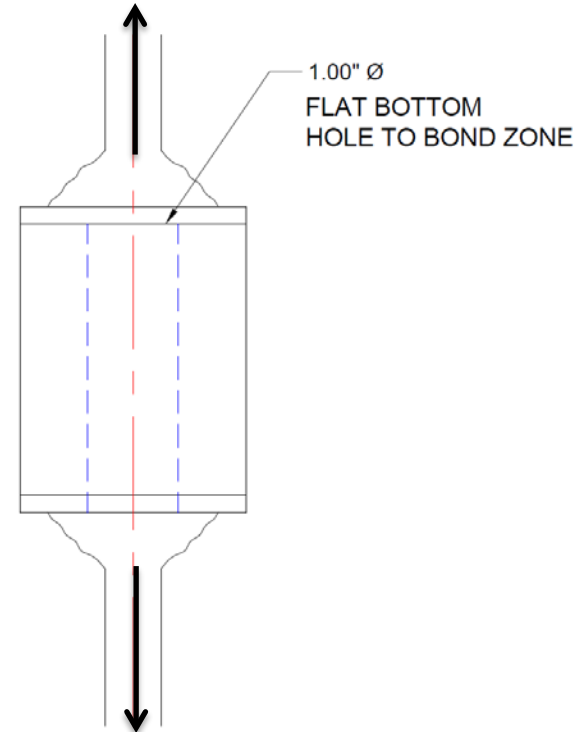


No clad
separation
or disbond



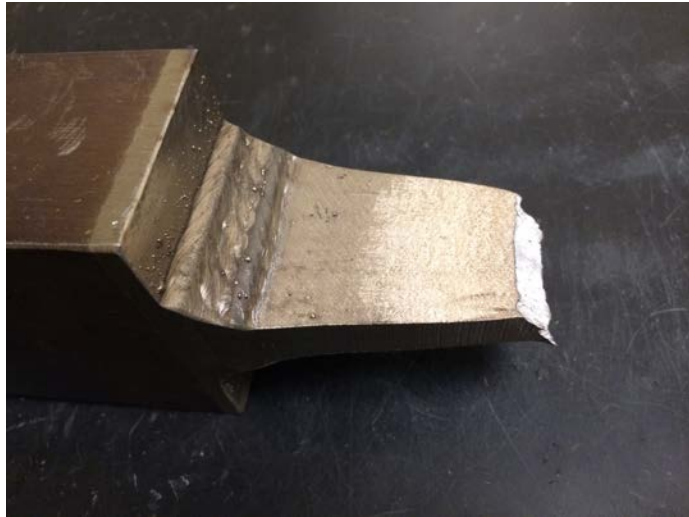
TENSILE TESTING WITH SIMULATED NON-BOND IN CLADDING

- Application mock-up testing
 - 25mm flat bottom hole drilled to the interface to simulate a 25mm non-bond.



TENSILE TESTING WITH SIMULATED NON-BOND IN CLADDING

Load at Break = 525 kN
No disbond at simulated non-bond





COMPARATIVE TENSILE AND SHEAR STRENGTH OF EXPLOSION CLAD MATERIALS

Conclusions

- The clad tensile strength exceeded the shear strength for 100% of the materials tested
- The through thickness tensile strength of explosion welded titanium alloy and copper alloy clad are well above the cladding metal minimum tensile strengths
- For explosion welded stainless steel and nickel alloy clad, the tensile strength of explosion weld
 - Exceeded the tensile strength of the steel base metal and
 - Meets the base metal minimum tensile strength requirement.
 - Tensile strength maintained for thinner cladding metal, welded test coupons, with various heat treatment conditions, and at elevated temperature
 - Mock-up testing did not produce any clad separation or disbonding





COMPARATIVE TENSILE AND SHEAR STRENGTH OF EXPLOSION CLAD MATERIALS

Conclusions

- Tensile strength data of NobelClad EXW material supports direct attachment to the clad surface



Thank you

Curtis Prothe

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