

(Hot) Explosive cladding of tungsten on copper and stainless steel substrates

EPNM-2008, Lisse, The Netherlands

TNO | Defence, Security and Safety



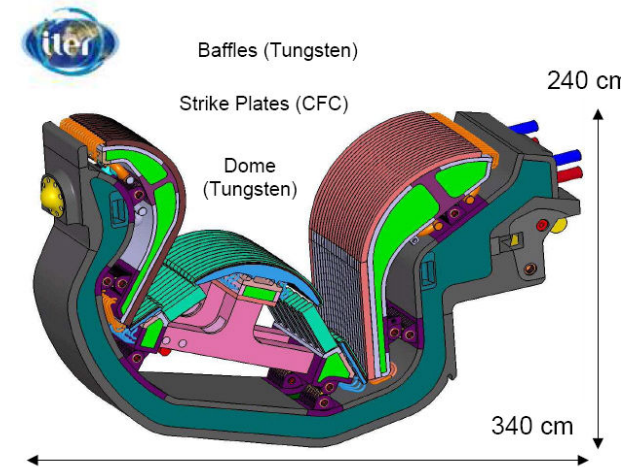
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Petten (NL)

Content

- Background
- Foil cladding
- Hot cladding
- Conclusions



W coating for ITER reactor wall parts



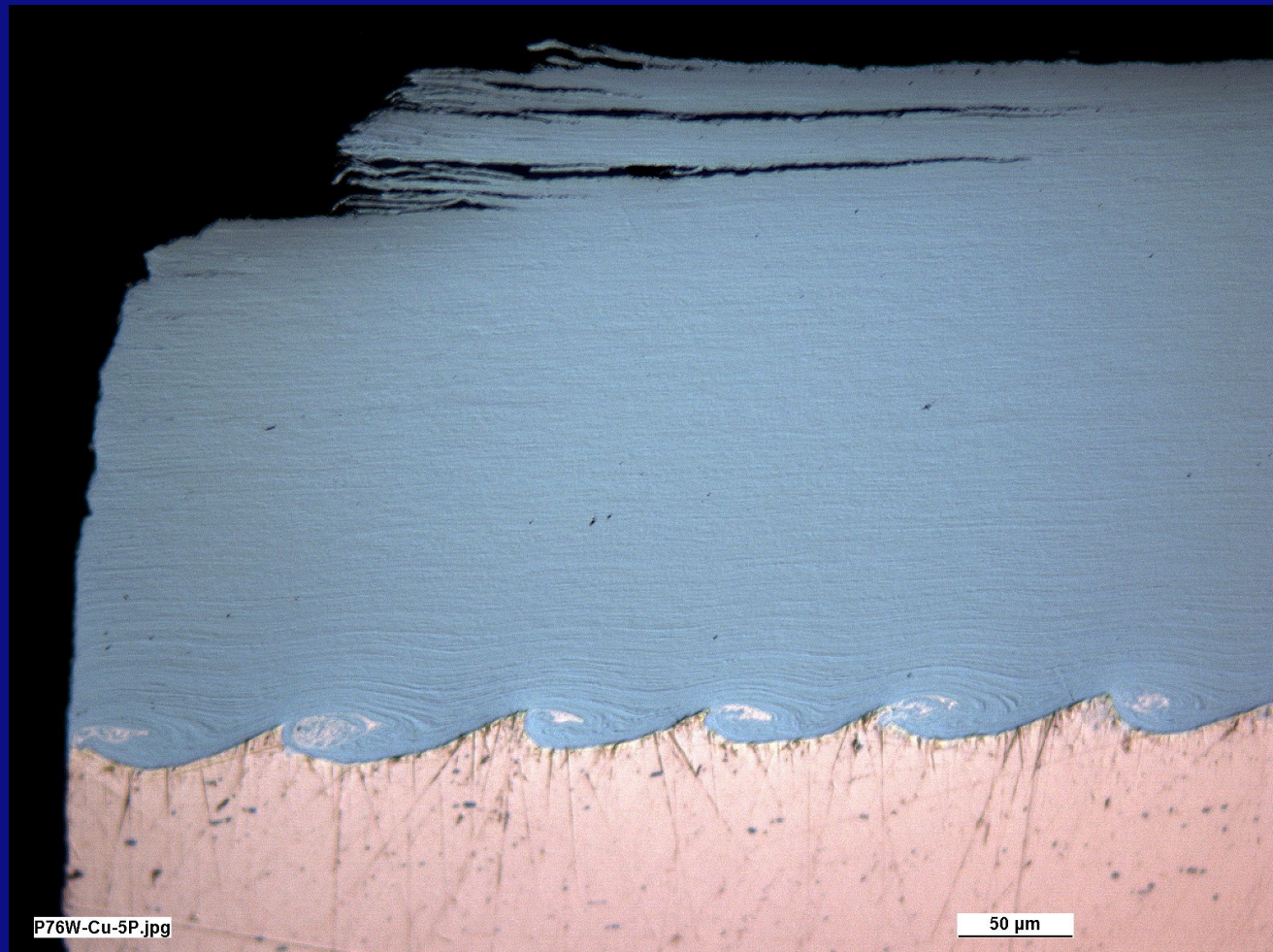
- Rationale for W as armor on wall parts (heat exchangers)
 - high melting point, high heat conductivity, high Z, nuclear properties acceptable

- EFDA¹ feasibility study with NRG –
 - W by explosion bonding 1-2 mm on Cu and ss for heat exchangers? - brittleness, no intermetallics² →

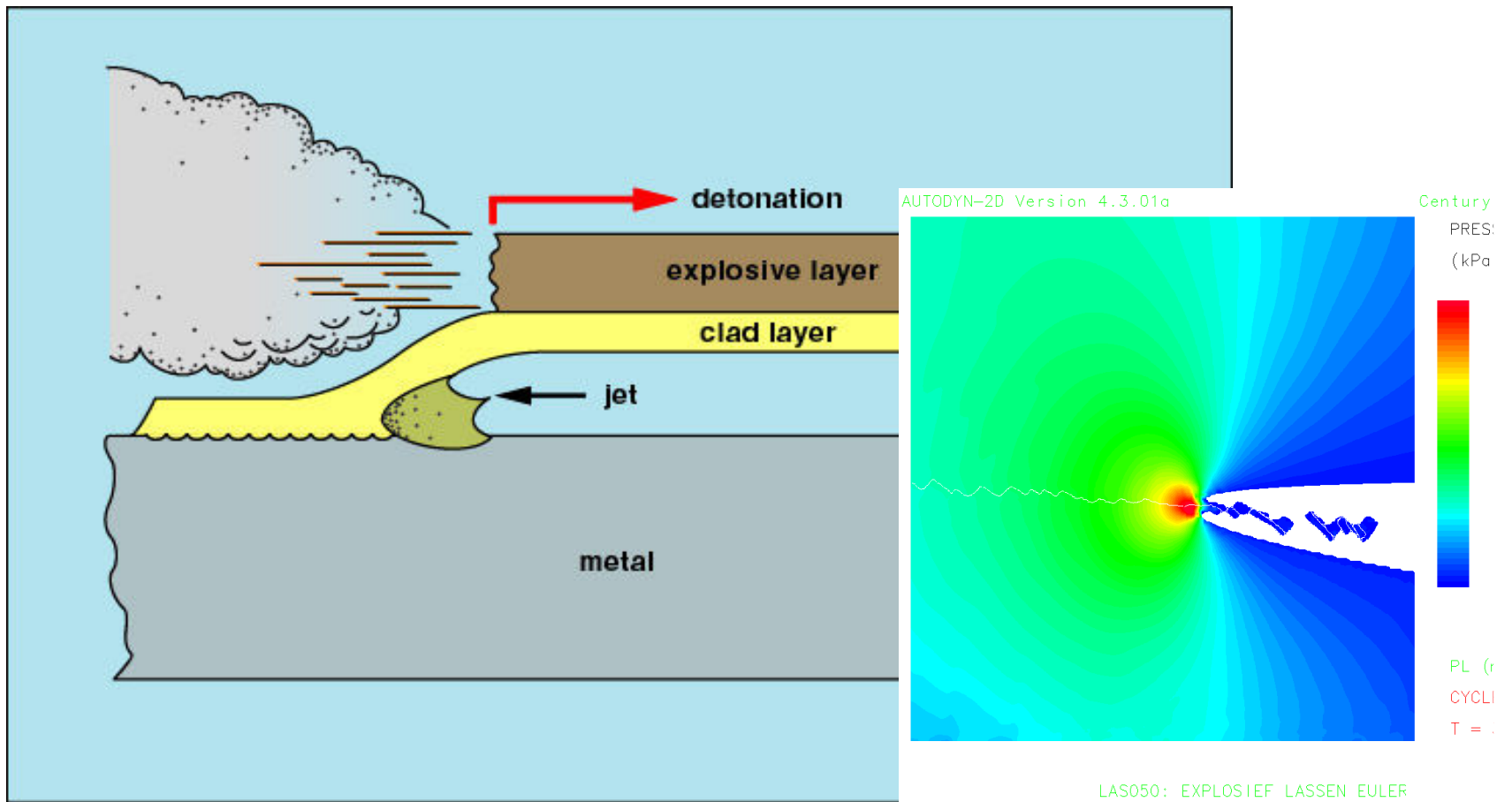
2) A. Oberg et al. Metallurgical Trans. A, Vol. 16 A, p. 841, (1985)

1) This work was partly supported by the Dutch Government in the framework of the 2006 ITER-UPL project and by the EC under the Contract of Association A 4323 between EURATOM-FOM.

W (0.3 mm) brittleness and ductility under high impact
No intermetallic phase between W and Cu (Miedema model)

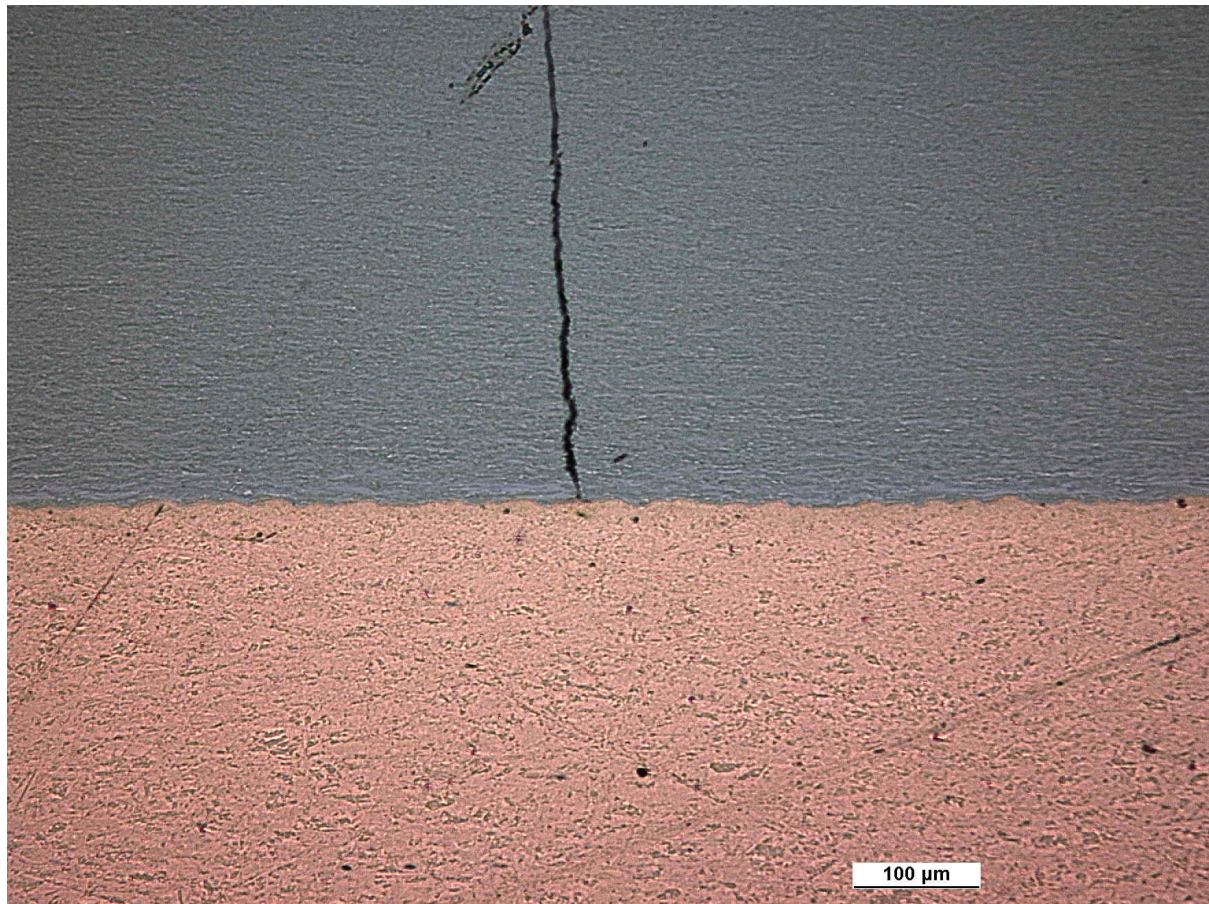


Explosive cladding with pressure modelling
(look at jet!)



Cu flyer (3 mm) onto W base (1 mm) –
containment - self-castellation

(I17)

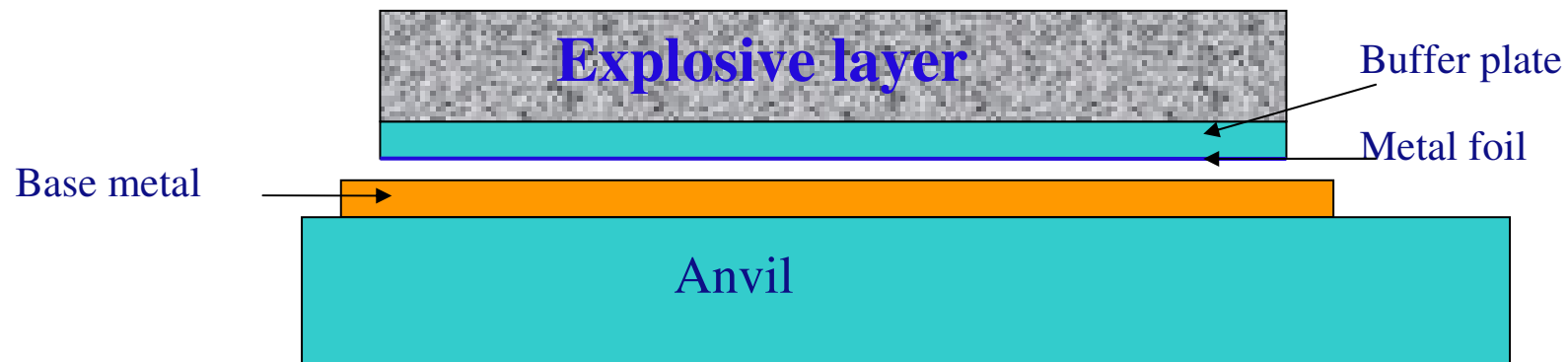


Multiple foil cladding (2 x 0.5 mm/ 3 x 0.3 mm)



Foil cladding

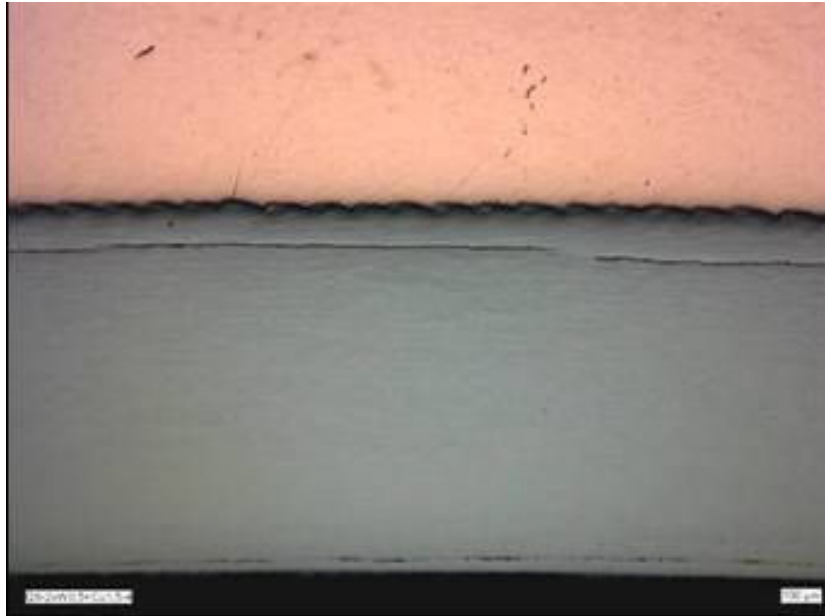
- Foil attached to buffer plate
- Same process as cladding thicker plates
- Buffer does not bond (no inclined impact)



Multiple clad (3 x 0.3 mm W) – spall (I23)



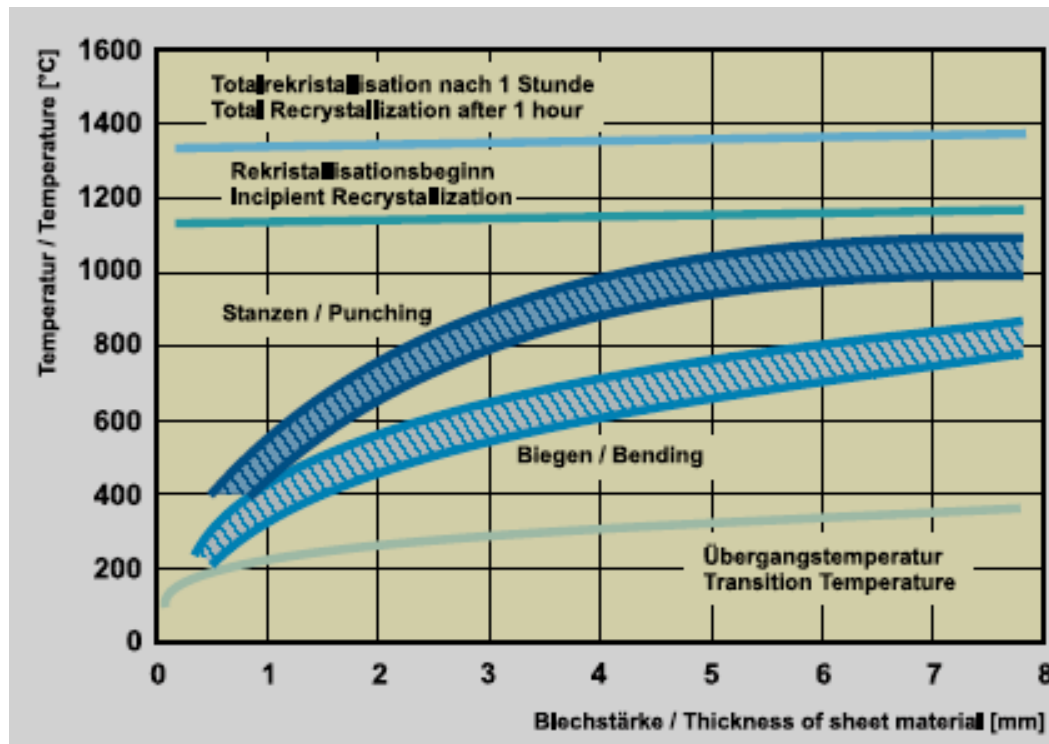
Cu (flyer) onto 2 x W foils (0,5 mm) – /28



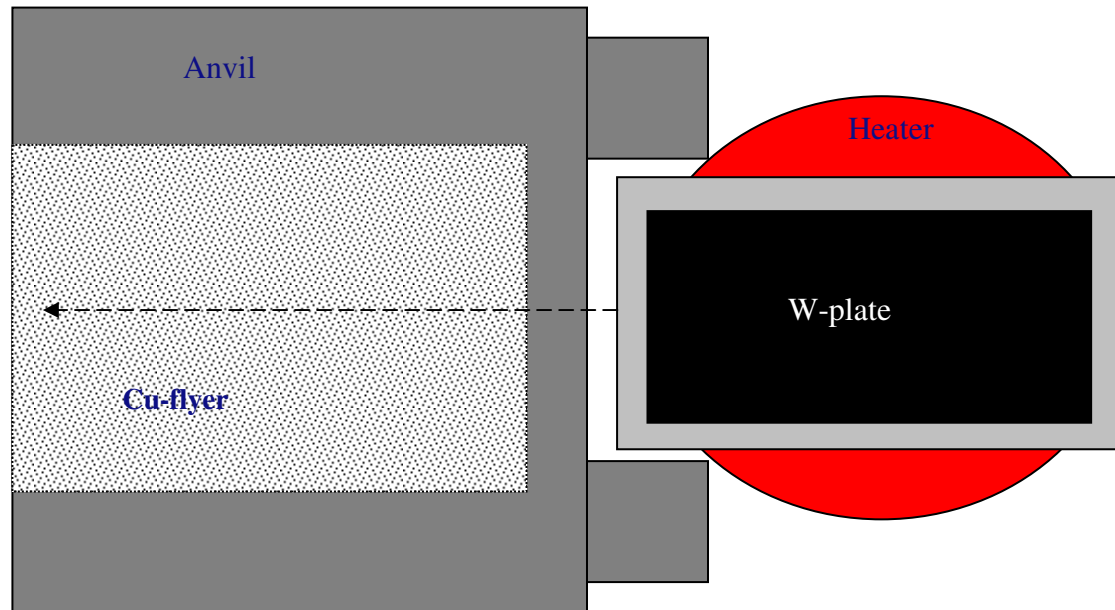
Cladding at elevated W temperature



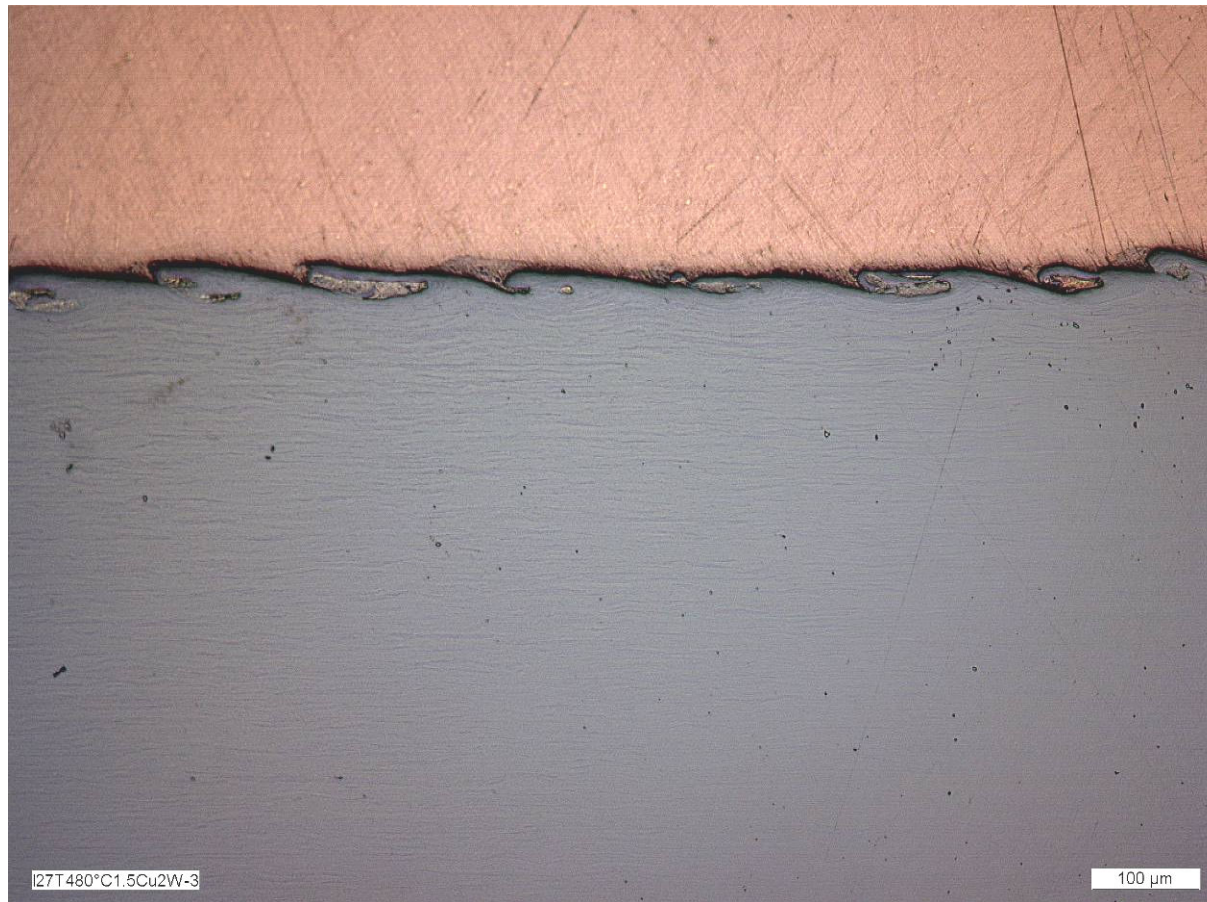
Ductile to brittle temperature (T_{DTBT})— versus W metal thickness (Plansee SE)



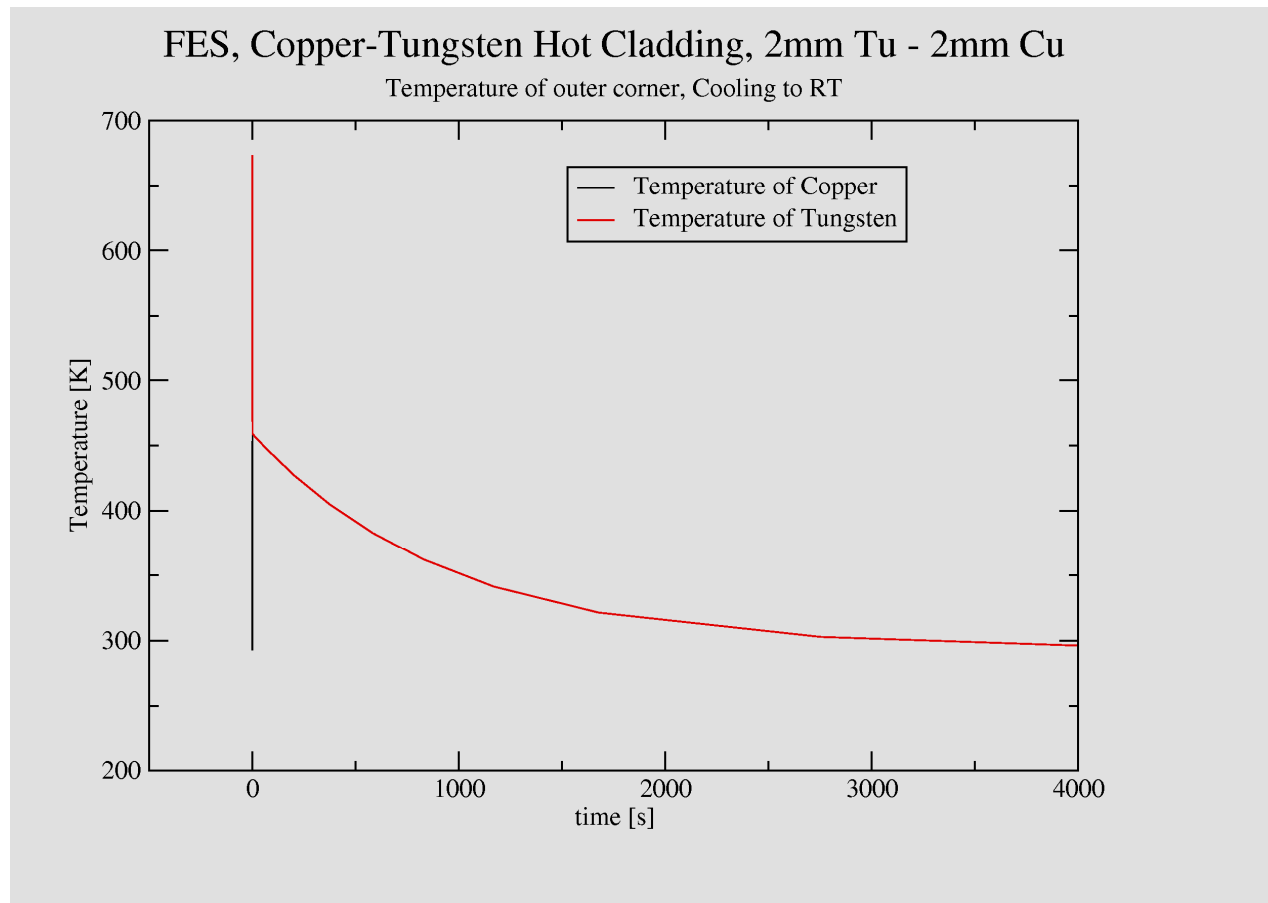
Set-up for hot cladding of Cu onto W – type I (pull and draw)



Cu clad onto 2 mm W at 480 deg C – no cracks I27



Hot cladding vs. Thermal stresses

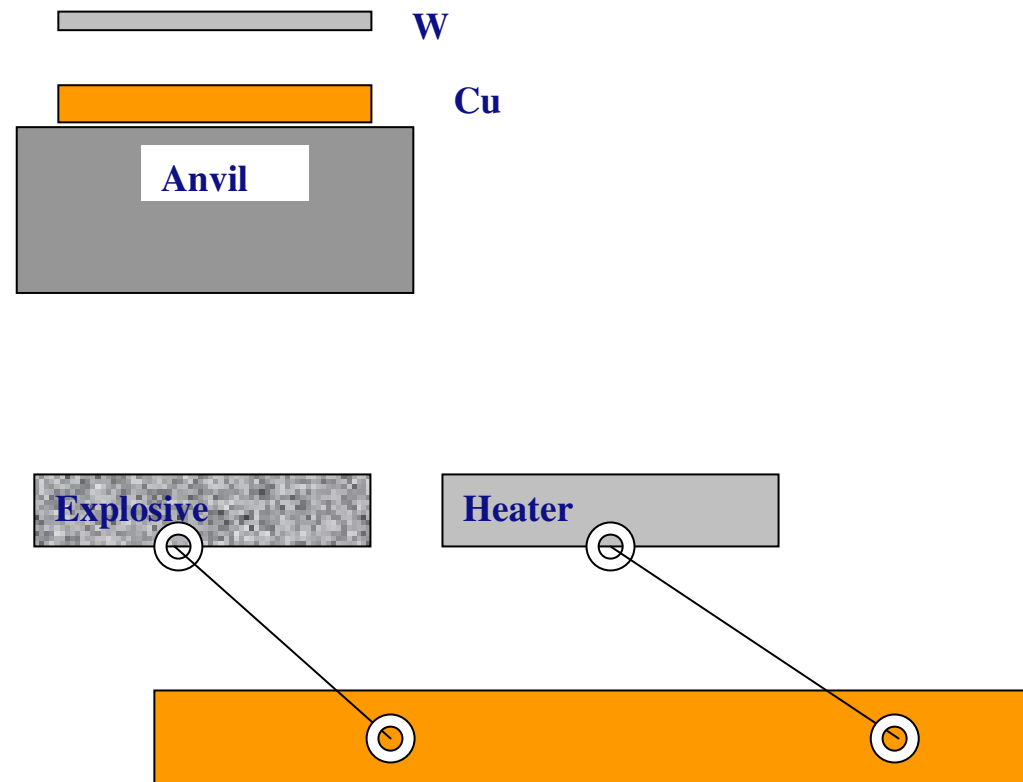


Hot cladding - W heated above T_{DBTT}

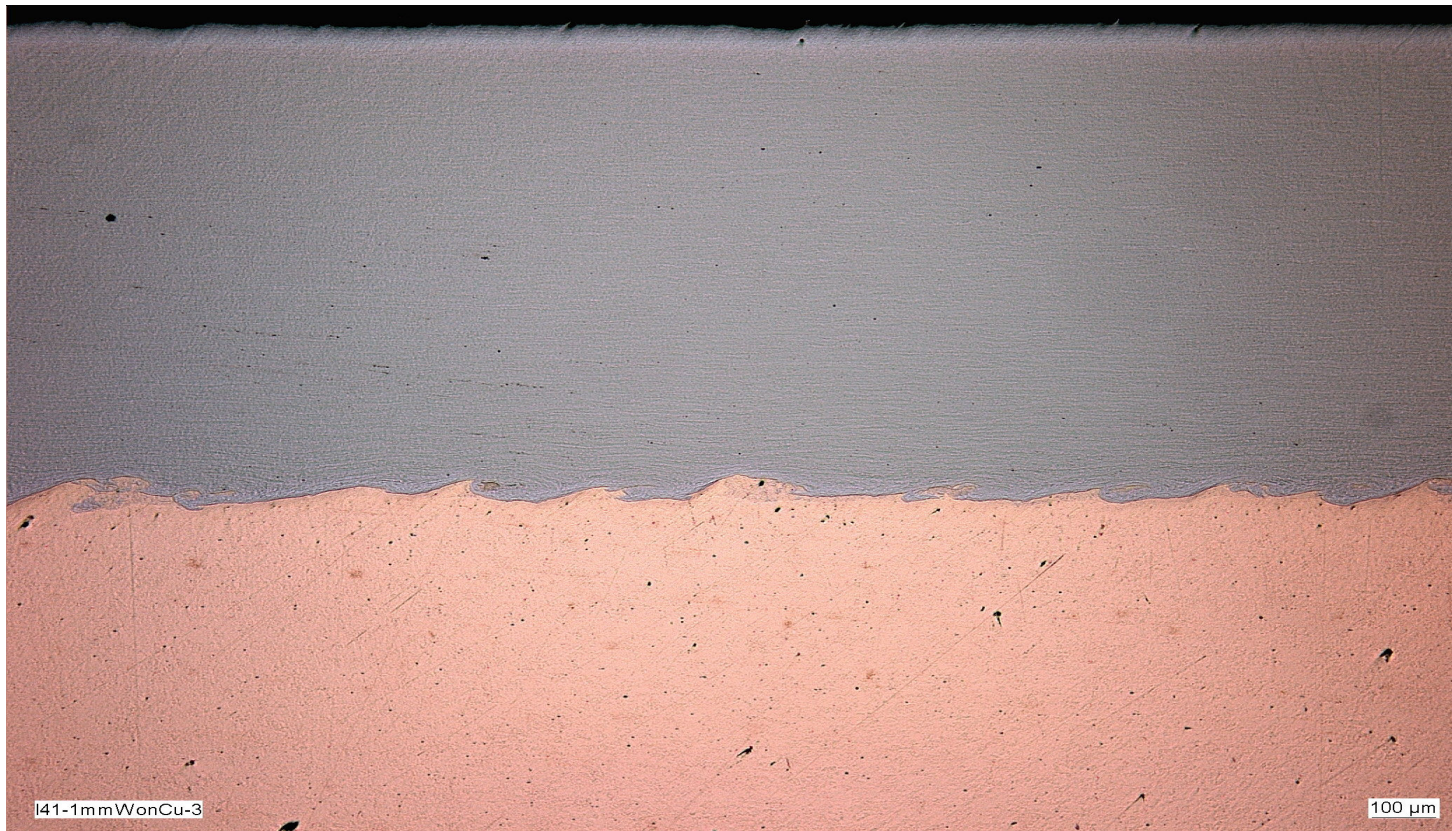
- W clad onto Cu, CuCrZr and stainless steel (316) - selection

| No | flyer metal | flyer (mm) | flyer T (deg C) | base metal | base (mm) | base T (deg C) | Quality | Interface s (MPa) | T (eq) (deg C) | d_{Cu} / d_W |
|------|----------------|---------------|-----------------------|---------------|--------------|----------------------|---------|-------------------------|-------------------|----------------|
| I27 | Cu | 1.5 | | W | 2 | 480 | + | 1016 | 246 | 0.75 |
| I34 | SS 316 | 2.5 | | W | 2 | 500 | + | 465 | 192 | 1.25 |
| I36B | CuCrZr | 1.9 | | W | 2 | 500 | + | 935 | 228 | 0.95 |
| I44 | Cu | 1.5 | | W | 2 | 500 | + | 1061 | 256 | 0.75 |
| I45 | Cu | 3 | | W | 2 | 550 | + | 777 | 193 | 1.5 |
| I41 | W | 1 | 500 | Cu | 5 | 65 | + | 450 | 120 | 5 |
| I31 | Cu | 1.5 | | W | 5 | 500 | x | 1623 | 381 | 5 |

Set-up for hot cladding of W onto Cu – type hinge



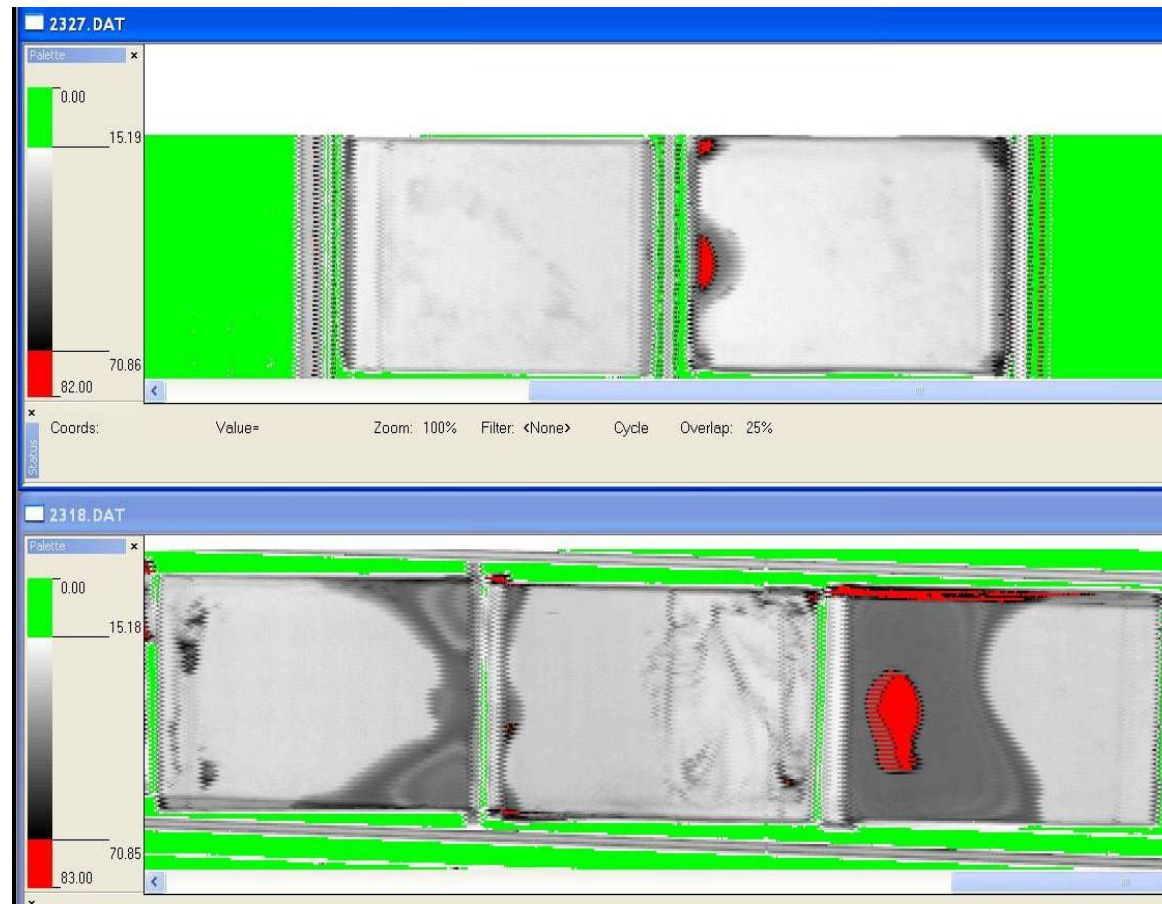
W clad (1 mm) onto Cu (5 mm) - W is the hot flyer!
(I41)



W clad (1 mm) onto Cu (5 mm) - W used as hot flyer
cont. (I41)

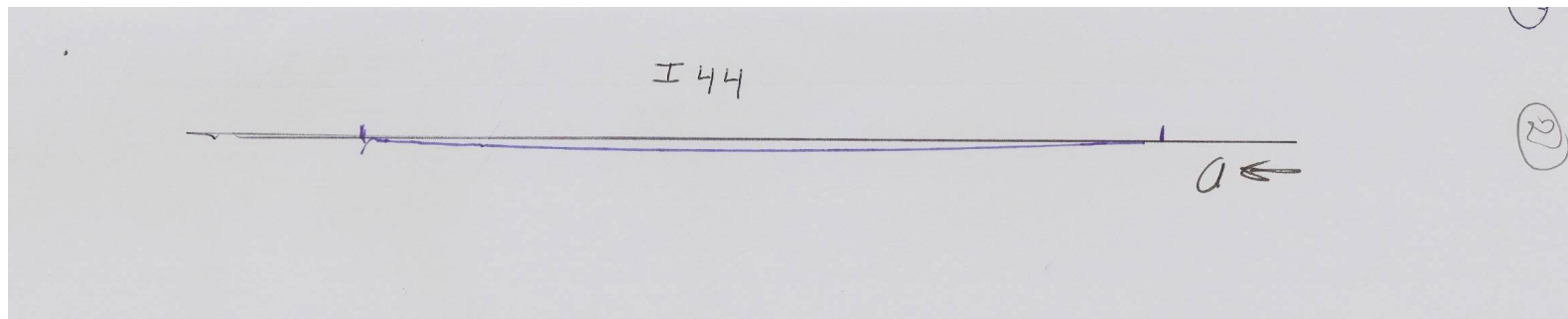


Analysis (I) – C scans - W clad (1.5-3 mm) onto Cu

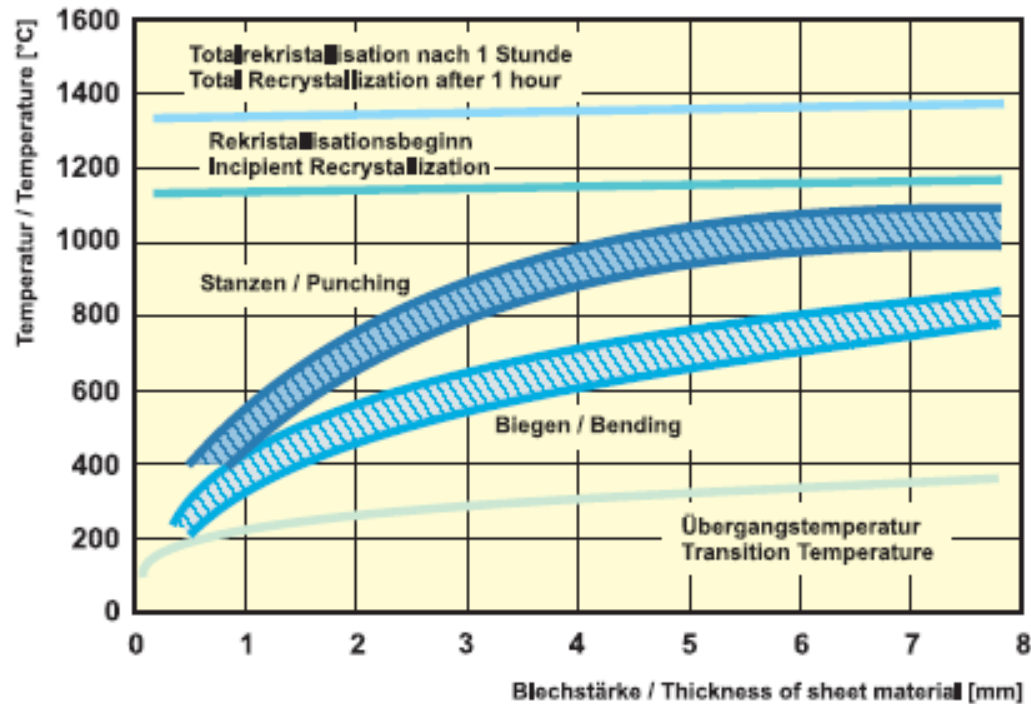


Analysis (2)

- 2 mm W onto 1,5 mm Cu (OFHC) - I44 blue is copper
- 2 mm W onto 3 mm Cu (OFHC) - I45 opposite curvature
- Flatness could be improved by hot pressing at about 500 deg C, see Plansee datasheet for “Biegen”
- W clad will be castellated for mock-up testing (heat flux)



W temperature for “Biegen” – 450-550 degC



Conclusions

- W foil (0, 3 mm) can be clad onto Cu at room temperature (to cover larger side sections of divertor?)
- Multiple foil cladding is not appropriate (parallel cracks)
- Hot cladding has given good results – 1-2 mm W onto Cu, CuCrZr and SS (ca. 2 mm)

Further analysis of interface by NRG (interface) and processing for mock-up testing (EFDA) to be done

